

# De rol van modelparameters in het Soft Soil Creep model

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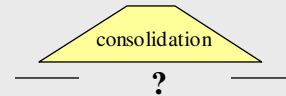
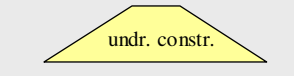
## Introduction

Observation during embankment construction and consolidation:

- Lateral displacements away from the embankment toe

FE calculations tend to show:

- During undrained construction: lateral displacements away from the embankment toe
- During consolidation: lateral displacements towards the embankment toe (lateral confinement)



## Introduction

Lateral confinement is unrealistic and results from the use of simplified constitutive models where Hooke's law plays a dominant role

Solutions to improve lateral displacements:

- Anisotropy (Ladd et.al., 1994)
- Creep (this contribution)
- Hardening plasticity (?)



# Soft Soil Creep model

$$\dot{\epsilon}_v = \dot{\epsilon}_v^e + \dot{\epsilon}_v^c = \frac{\kappa^*}{p'} \dot{p}' + \frac{\mu^*}{\tau} \left( \frac{p^{eq}}{p_p^{eq}} \right)^{\frac{\lambda^* - \kappa^*}{\mu^*}}$$

$$p^{eq} = p' + \frac{q^2}{M^2 p'}$$

$$p_p^{eq} = p_p^0 \exp\left(\frac{-\epsilon_v^c}{\lambda^* - \kappa^*}\right)$$

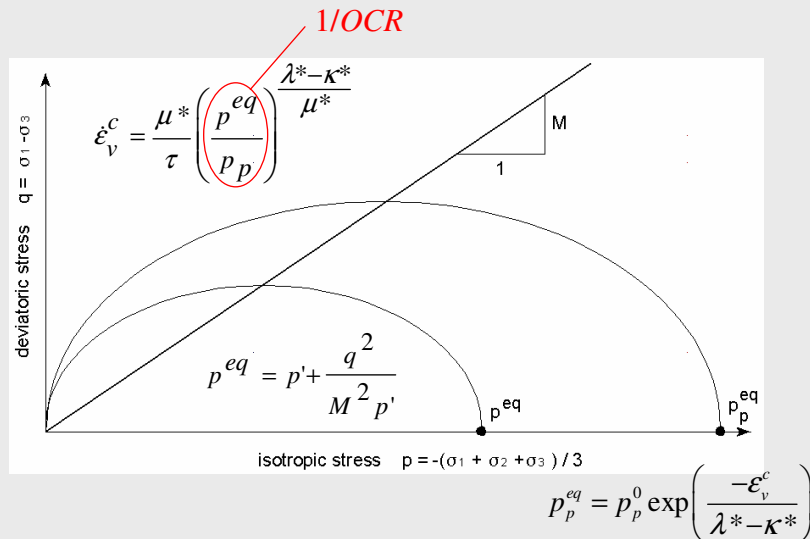
$$\epsilon_v^c = \int \dot{\epsilon}_v^c dt$$

Parameters:

- $\kappa^*$  = Modified swelling index
- $\lambda^*$  = Modified compression index
- $\mu^*$  = Modified creep index
- $\nu_{ur}$  = Poisson's ratio for unloading / rel.
- $\tau$  = Intrinsic time parameter (1 day)
- $M$  = Steepness of the creep contour
- $p_p$  = Isotropic preconsolidation stress



# Soft Soil Creep model

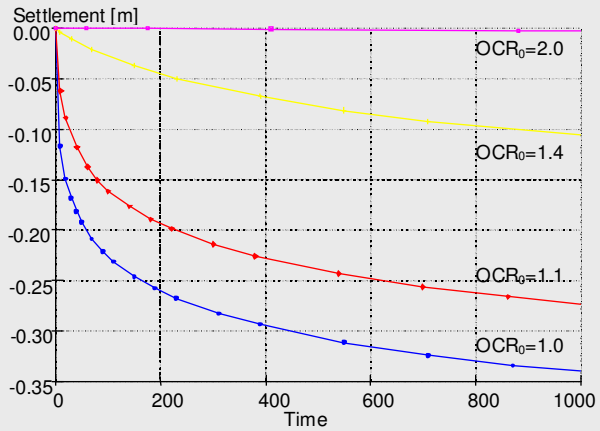


# One-dimensional compression

Influence of initial OCR on settlement of a 10m thick layer with initial stresses:



$\gamma = 17 \text{ kN/m}^3$   
 $\kappa^* = 0.02$   
 $\lambda^* = 0.10$   
 $\mu^* = 0.005$   
 $\nu_{ur} = 0.15$   
 $\phi' = 26^\circ$   
 $c' = 1 \text{ kN/m}^2$   
 $K_0^{nc} = 0.70$   
 $K_0 = 0.70$



# One-dimensional compression

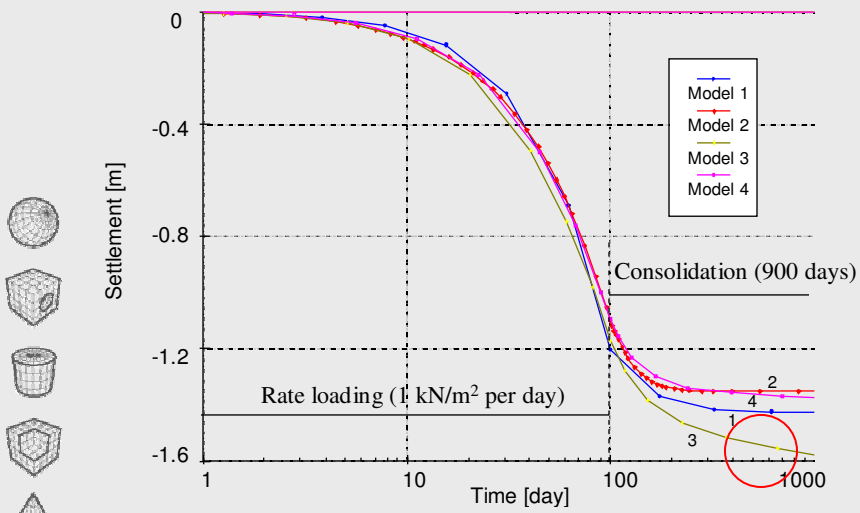
10 m thick undrained clay layer with initial stresses ( $K_0=0.72$ )



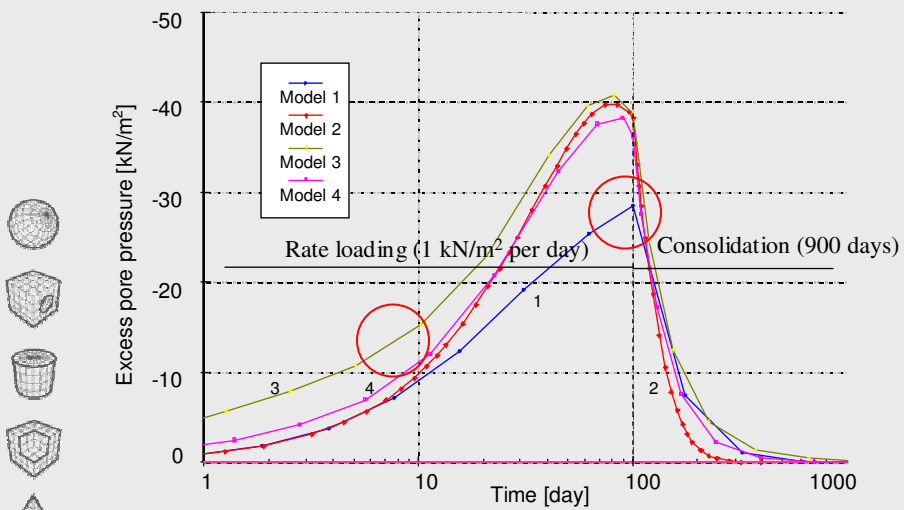
Model 1	Model 2	Model 3	Model 4
Mohr-Coulomb	Modified Cam-Clay (Soft Soil)	Soft Soil Creep	Soft Soil Creep
$E_{ref} = 50 \text{ kN/m}^2$	$\lambda^* = 0.10$	$\lambda^* = 0.10$	$\lambda^* = 0.10$
$E_{inc} = 150 \text{ kN/m}^3$	$\kappa^* = 0.02$	$\kappa^* = 0.02$	$\kappa^* = 0.02$
		$\mu^* = 0.004$	$\mu^* = 0.001$
$\nu' = 0.35$	$\nu_{ur} = 0.15$	$\nu_{ur} = 0.15$	$\nu_{ur} = 0.15$
	$M = 0.99$	$M = 0.99$	$M = 0.99$
	$OCR_0 = 1.0$	$OCR_0 = 1.0$	$OCR_0 = 1.0$

$\gamma = 15 / 18 \text{ kN/m}^3$      $\phi = 25^\circ$      $c = 1 \text{ kN/m}^2$      $k = 10^{-2} \text{ m/day}$

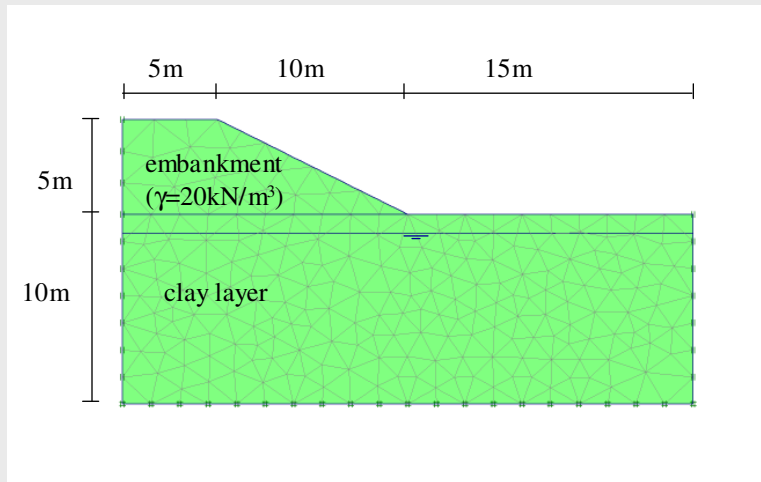
# One-dimensional compression



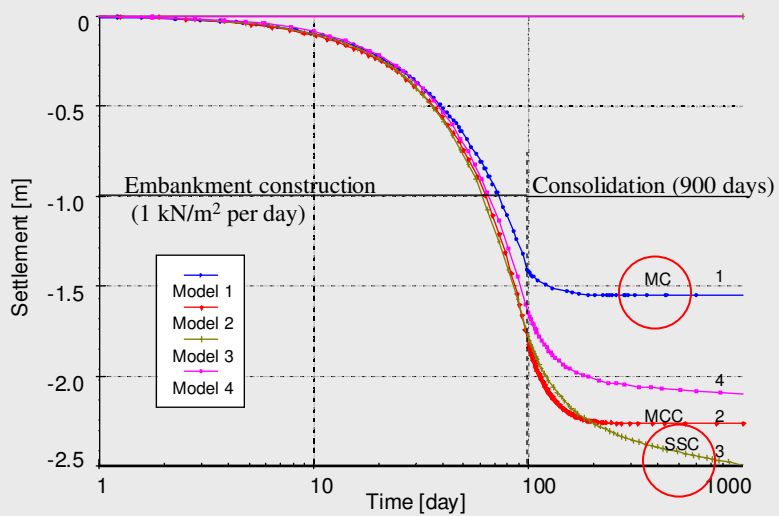
# One-dimensional compression



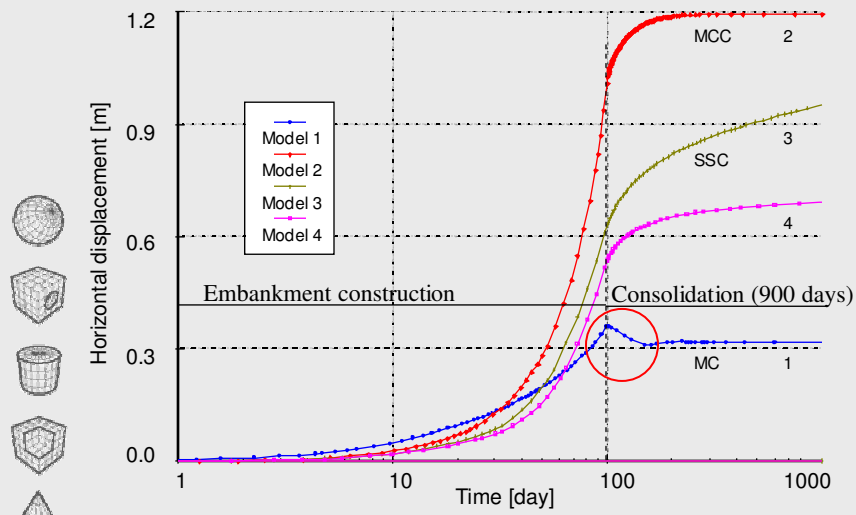
# Embankment construction



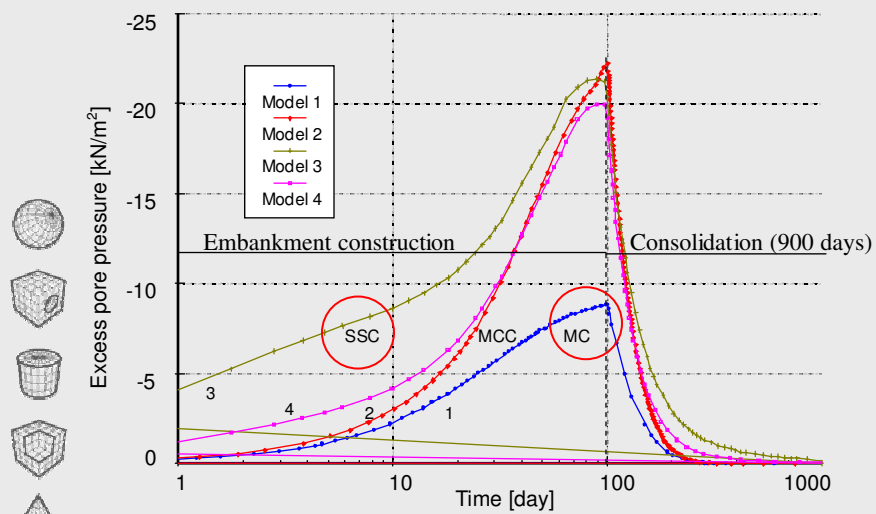
# Embankment construction



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# Embankment construction



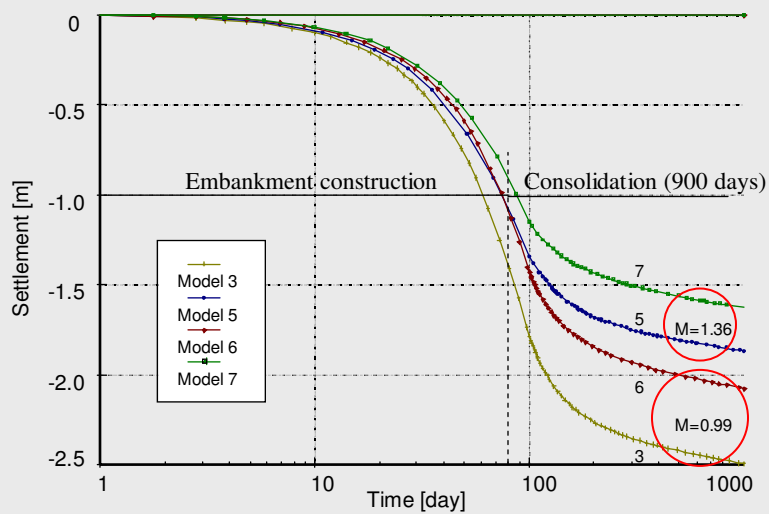
## Variation of $M$ ( $K_0^{nc}$ ) and $OCR_0$

Model 3	Model 5	Model 6	Model 7
Soft Soil Creep	Soft Soil Creep	Soft Soil Creep	Soft Soil Creep
$\lambda^*=0.10$	$\lambda^*=0.10$	$\lambda^*=0.10$	$\lambda^*=0.10$
$\kappa^*=0.02$	$\kappa^*=0.02$	$\kappa^*=0.02$	$\kappa^*=0.02$
$\mu^*=0.004$	$\mu^*=0.004$	$\mu^*=0.004$	$\mu^*=0.004$
$v_{ur}=0.15$	$v_{ur}=0.15$	$v_{ur}=0.15$	$v_{ur}=0.15$
$M=0.99$	$M=1.36$	$M=0.99$	$M=1.36$
$OCR_0=1.0$	$OCR_0=1.0$	$OCR_0=1.3$	$OCR_0=1.3$

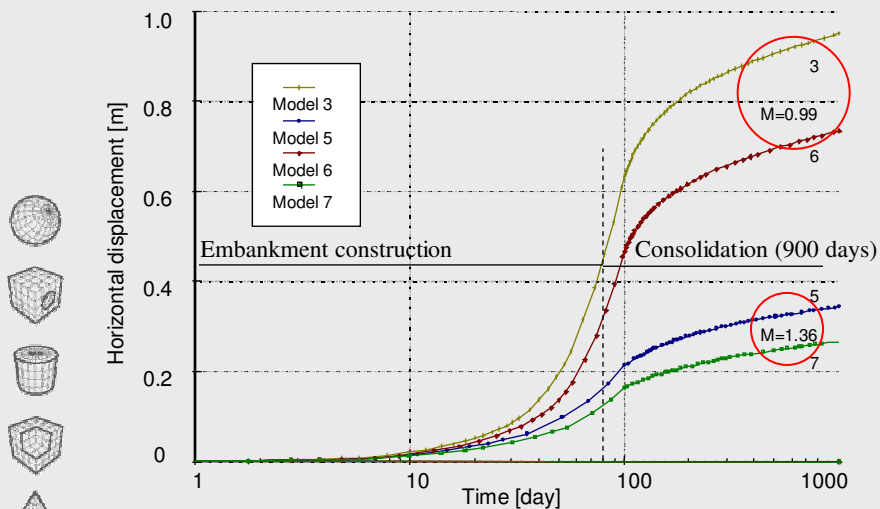
$M = 0.99$ : standard for SSC model       $M = 1.36$ : standard for SS model



## Variation of $M$ and $OCR_0$



## Variation of $M$ and $OCR_0$



## Conclusions

- Lateral confinement under embankment during consolidation (MC) can be overcome by creep.
- The MC model gives lower excess pore pressures than the MCC(SS) and the SSC model.
- For realistic values of the creep index, the SSC model gives larger (time-dependent) settlements than the MCC(SS) model.
- For low (unrealistic) values of the creep index, the SSC model gives similar settlements as the MCC(SS) model.
- The settlements due to embankment construction are larger than due to one-dimensional compression with the same maximum load.

## Conclusions (cont.)

- The  $M$ -parameter (steepness of the Cap) in the SSC model is crucial for lateral displacements:
  - Low value (based on friction; default in Plaxis V8)
    - > Displacements too large
  - High value (based on proper  $K_0^{nc}$ ; default for SS model)
    - > Reasonable displacements
- The initial  $OCR$ -value in the SSC model should generally be selected larger than 1.0 for NC-clays to get realistic initial creep strain rates (settlements and horizontal displacements)



Thank you for your attention...

Questions ?



**Reference:**

Brinkgreve, R.B.J., (2004). *Time-dependent behaviour of soft soils during embankment construction – a numerical study*. Proc. NUMOG IX, pp.631-637